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# Phase-engineered low-resistance contacts for ultrathin MoS<sub>2</sub> transistors

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Ultrathin molybdenum disulphide (MoS₂) has emerged as an interesting layered semiconductor because of its finite energy bandgap and the absence of dangling bonds. However, metals deposited on the semiconducting 2H phase usually form high-resistance (0.7 kΩ μm-10 kΩ μm) contacts, leading to Schottky-limited transport. In this study, we demonstrate that the metallic 1T phase of MoS₂ can be locally induced on semiconducting 2H phase nanosheets, thus decreasing contact resistances to 200-300  $\Omega$  μm at zero gate bias. Field-effect transistors (FETs) with 1T phase electrodes fabricated and tested in air exhibit mobility values of  $\sim\!50$  cm² V $^{-1}$  s $^{-1}$ , subthreshold swing values below 100 mV per decade, on/off ratios of  $>\!10^7$ , drive currents approaching  $\sim\!100$  μA μm $^{-1}$ , and excellent current saturation. The deposition of different metals has limited influence on the FET performance, suggesting that the 1T/2H interface controls carrier injection into the channel. An increased reproducibility of the electrical characteristics is also obtained with our strategy based on phase engineering of MoS₂.

he presence of a finite bandgap and excellent electrostatic gate coupling in ultrathin two-dimensional materials such as molybdenum disulphide (MoS<sub>2</sub>) make them interesting for electronics based on the current complementary metal oxide semiconductor (CMOS) paradigm<sup>1-10</sup>. Field-effect transistors (FETs) based on ultrathin MoS2 channels have been widely studied because they exhibit large on/off ratios and neartheoretical subthreshold swing values<sup>1,11–14</sup>. Efforts towards further optimization of devices through fundamental understanding have led to studies investigating the influence of contact electrodes, intrinsic limitations in transport of carriers, and techniques for improving the mobility of MoS2 devices15-24. Analysis of the literature reveals that mobility values, which are often used to demonstrate the quality of the material and devices, can vary from 1 to 400 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup>. The large deviation in mobility values arises from intrinsic challenges related to forming good contacts and differences in device fabrication and measurement procedures. For example, encapsulation of devices leads to substantial enhancement in mobility due to charge screening<sup>1,15,25,26</sup>. In the absence of encapsulation, removal of oxygen and water adsorbents via annealing<sup>27–29</sup>, or measurement of properties in good vacuum<sup>28,30-32</sup> also result in increased mobility values. Multilayered samples in excess of  $\sim$ 5 layers typically show higher mobility than thinner materials<sup>17,33</sup>.

Contact resistance is a key problem in ultrathin  $MoS_2$  (1–10 layers) devices owing to the formation of a Schottky barrier for electron injection. Performance of  $MoS_2$  FETs is strongly dependent on the metal used for source and drain electrodes<sup>17,18,34</sup>. In some studies, chemical interactions between the  $MoS_2$  nanosheet and sulphide-forming metals such as Ti have been shown to detrimentally impact the device properties<sup>10</sup>. The most common electrode material used in  $MoS_2$  FETs is gold, which in general yields reasonable device characteristics despite the large energy offset<sup>1,35,36</sup>. Detailed investigation of electrode materials with varying work functions has revealed that Fermi level pinning at the interface

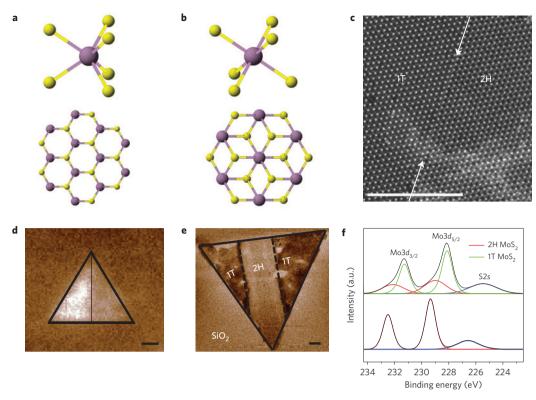
strongly impacts the device characteristics. Low-work-function metals with energy levels close to the conduction band of  $MoS_2$  enhance the device performance<sup>17</sup> as a result of efficient injection of carriers, which in turn decreases the contact resistance.

For high-performance electronics, ideal contact electrodes consist of trap-free interfaces, possess low contact resistance, and are ohmic. In modern silicon-based microelectronics, this is achieved by designing source and drain contacts that are based on degenerately doped n++ or p++ regions on which metal pads are deposited. Thus the contact material is a highly conducting version of the channel material so that the interface resistance is low, structural mismatch is limited, and injection of carriers is facilitated. Similar strategies are used in III–V semiconductor technologies. Applying existing state-of-the-art schemes to improve contact properties in FETs from two-dimensional materials is not straightforward because their atomically thin nature makes doping challenging. Surface modification by molecules and ions can locally alter the conductivity<sup>37</sup>, but such treatments suffer from long-term stability issues.

Here we demonstrate a new strategy based on phase engineering to design low-resistance contacts to realize FETs based on ultrathin MoS2 with enhanced performance. We have developed a methodology to locally pattern the metallic 1T phase on ultrathin semiconducting MoS<sub>2</sub> nanosheets and use them as electrodes. We demonstrate contact resistances of 200–300  $\Omega$   $\mu m$  at zero gate bias. The low contact resistance is attributed to the atomically sharp interface between the phases and to the fact the work function of the 1T phase and the conduction band energy relative to vacuum level of the 2H phase are similar (~4.2 eV). Both top- and bottom-gated devices with 1T electrodes show enhanced performance compared to devices in which metal is contacted directly to the semiconducting 2H phase. Specifically, we measure the properties in air and obtain mobility values of  $\sim 50 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ , subthreshold swing values of 90-100 mV/decade, and on/off ratios of  $>10^7$ . Furthermore, device performance with 1T electrodes is

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**ARTICLES** 



**Figure 1** | **1T** and **2H** phases of MoS<sub>2</sub>. **a,b**, Crystal structures of the 2H and 1T phases, respectively. In the upper diagram, trigonal prismatic (**a**) and octahedral (**b**) coordinations are shown. The lower panel shows the *c*-axis view of single-layer TMD with trigonal prismatic (**a**) and octahedral (**b**) coordinations. Atom colour code: purple, metal; yellow, chalcogen. **c**, High-resolution transmission electron microscope image of an atomically thin phase boundary (indicated by the arrows) between the 1T and 2H phases in a monolayered MoS<sub>2</sub> nanosheet. Scale bar, 1 nm. **d**, Photoluminescence map of a triangular monolayered MoS<sub>2</sub> nanosheet. The left side of the triangle is the 2H phase, whereas the right side was converted to the 1T phase. The 2H phase shows noticeably brighter PL than the 1T phase. **e**, Electrostatic force microscopy phase image of a monolayered MoS<sub>2</sub> nanosheet showing the difference between locally patterned 2H (bright colour) and 1T (dark colour) phases. Scale bars in **d**,**e** are 1 μm. **f**, XPS spectra showing the Mo3*d* and S2s peaks of the 1T and 2H phases of MoS<sub>2</sub>. Typical experimentally measured spectra are shown in black and fits are shown in red (for the 2H phase component) and green (for the 1T phase component). The lower curve is 100% 2H phase, whereas the top curve can be fitted with both 1T and 2H phase components.

highly reproducible and independent of the type of contact metal pads used.

We have recently demonstrated the exfoliation of transition metal dichalcogenides (TMDs) such as MoS2 and WS2 (refs 38,39) using the well-known organolithium chemical method<sup>40,41</sup>. This synthesis route leads to the formation of the metallic 1T phase<sup>38,42,43</sup>. It has been shown that the 1T phase is stabilized by electron donation from the organolithium during intercalation 42,44-46. As shown in previous studies by others<sup>47–50</sup>, we have also demonstrated that the 1T phase is maintained even after complete removal of organolithium<sup>38,39</sup>. The 1T phase is metastable, with a relaxation energy of  $\sim$ 1.0 eV for conversion to the thermodynamically stable 2H phase  $^{39,51,52}$ . The crystal structures of the 2H and 1T phases are shown in Fig. 1a,b. High-resolution transmission electron microscopy has revealed that the 1T and 2H phases can coexist in the same TMD nanosheets and that the phase boundary between the two phases is atomically sharp with no visible defects, as shown in Fig. 1c (ref. 53). Local and patterned conversion of the semiconducting 2H phase to the metallic 1T phase is shown in Fig. 1d,e. The photoluminescence (PL) map of a chemical-vapour-deposited single-layer triangle of MoS<sub>2</sub> that has been partially converted to the 1T phase is shown in Fig. 1d. PL is substantially quenched in the region that has been converted to the 1T phase. The concentration of the 1T phase in the converted region was obtained by X-ray photoelectron spectroscopy (XPS) and found to be  $\sim$ 60–70%, as shown in Fig. 1f (ref. 38). An electrostatic force microscopy (EFM) phase image of a micro-scale patterned 1T/2H/1T MoS<sub>2</sub> nanosheet is shown in Fig. 1e. The colour contrast

in EFM arises from conducting and non-conducting regions on the single-layer nanosheet. The results in Fig. 1d,e indicate that local patterning of the 1T phase on 2H nanosheets is possible and the interface between the phases is sharp. The electronic properties of the 1T phase show that it is metallic, with an estimated carrier concentration of  $>10^{13}$  cm $^{-2}$ . The high electron density and metallic nature of the phase is also demonstrated by the fact that gate modulation in the 1T phase is absent, as shown in Fig. 3a.

All FET devices reported in this study were fabricated on mechanically exfoliated ultrathin nanosheets of MoS<sub>2</sub> (obtained from SPI) with thicknesses ranging from one to three layers on 100 nm of SiO<sub>2</sub>/Si substrates. Source and drain electrodes were defined by lithographic patterning of the 1T phase, in which regions for conversion were left exposed while covering other regions with polymethylmethacrylate (PMMA). The uncovered regions were then treated with n-butyl lithium at room temperature for 1 h in a glove box (see Supplementary Information for details). The organic butyl residue and lithium ions were removed after treatment through thorough washing with hexane and de-ionized water, respectively<sup>38</sup>. The absence of lithium was confirmed by both electron energy-loss spectroscopy (EELS) in a scanning transmission electron microscope, as well as nuclear reaction analysis (NRA) shown in Supplementary Figs 9 and 10. Metal pads were then deposited on top of the 1T phase regions. After the 1T conversion, both top- and bottom-gated devices were processed (metal pad deposition and high k dielectric deposition) in exactly the same manner and simultaneously. Optical images of typical

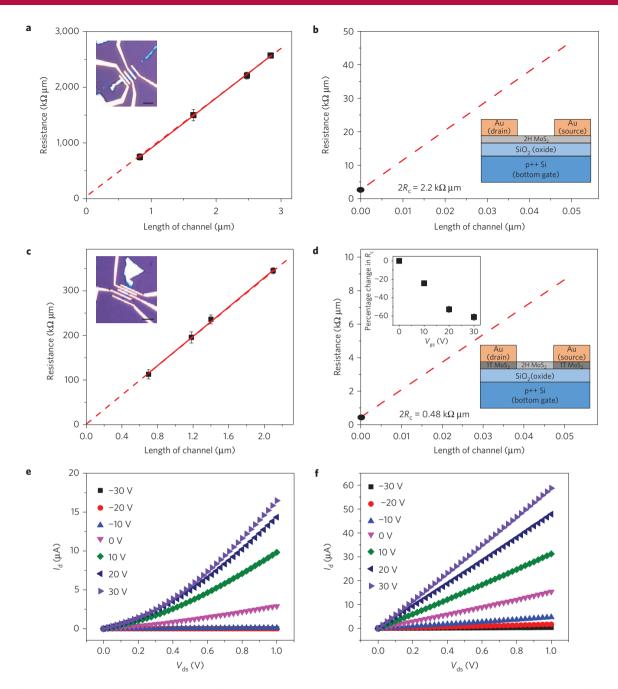


Figure 2 | Contact resistance of 1T and 2H phases. a-d, Resistance versus 2H channel lengths for Au deposited directly on the 2H phase (a,b) and on the 1T phase (c,d). Extrapolation of the red lines yields contact resistances ( $R_c$ ) of 1.1 kΩ μm for 2H (b) and 0.2 kΩ μm for 1T (d) contacts at zero gate bias. Inset in d shows the percentage decrease in contact resistance with gate bias. Optical microscope images and device schematics are also shown. Scale bars in device photos are 5 μm. The channel in 1T electrode devices is shorter than in 2H devices owing to the diffusion of butyl lithium into the masked region. The error bars in a,c result from averaging of least five measurements on at least three devices. e,f, Drain current ( $I_d$ ) characteristics of back-gated FETs for 0-1 V drain-source voltages ( $V_{ds}$ ) and gate-source voltages  $V_{gs}$  ranging from -30 V to 30 V, showing Schottky behaviour for gold directly onto the 2H phase (e) and linear behaviour for the 1T electrodes (f).

devices are shown in Fig. 2. Top-gated devices were investigated through deposition of high k dielectrics by atomic layer deposition (ALD) or plasma-enhanced chemical vapour deposition (PECVD; see Supplementary Information for details).

The contact resistances were measured using the transfer length method (TLM), as shown in Fig. 2a–d. We tested two types of devices, shown schematically in Fig. 2b,d: ones in which the Au metal pads were contacted to the 1T phase and others in which the metal pads were contacted to the 2H phase directly. In both cases, the channel consisted of the 2H phase. To obtain good statistical

analyses, at least 25 samples were measured and analysed. As with all electrical measurements reported in this work, the TLM resistances were measured in air and no annealing was performed. It can be seen from Fig. 2 that the resistance of the 1T contacts decreases by a factor of  $\sim\!5$  from 1.1 k $\Omega$   $\mu m$  to 0.2 k $\Omega$   $\mu m$  at zero gate bias. The 1T contact resistance values are lower than the best values of  $\sim\!0.6-0.7$  k $\Omega$   $\mu m$  reported thus far for MoS $_2$  devices  $^{5,7,8,54}$ . It also compares very favourably with the current state-of-the-art metal/silicon contacts in CMOS technology  $^{55}$  (ITRS 2012 states source/drain parasitic resistance is in the range 0.3–0.5 k $\Omega$   $\mu m$  (290  $\Omega$   $\mu m$ , 405  $\Omega$   $\mu m$  and

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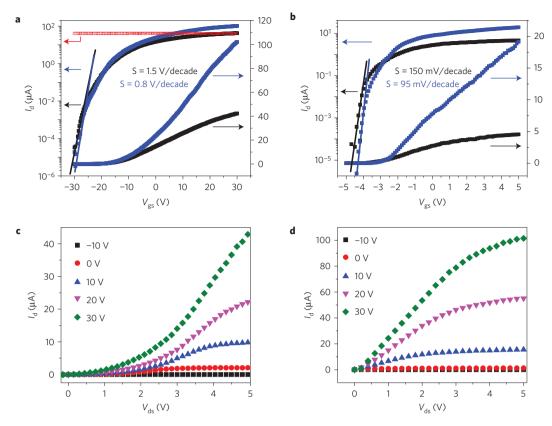


Figure 3 | Properties of field-effect transistors with 1T and 2H contacts. a,b, Transfer characteristics of bottom- and top-gated devices, respectively, measured at  $V_{ds} = 1$  V. (Logarithmic scale on the left and linear scale on the right.) Blue curves represent devices with 1T phase electrodes and the black curves are with Au on the 2H phase. The red curve in **a** is the  $I_d$  1T channel device, showing an absence of gate modulation owing to the metallic character of the 1T phase. The device width was 1.4  $\mu$ m and device length was 1.2  $\mu$ m. The linear fits used to extract the subthreshold swing values are also shown. **c.d.** Output characteristics of devices up to  $V_{ds} = 5$  V and  $V_{gs}$  ranging from -10 V to 30 V, showing reasonable saturation for Au (**c**) and 1T electrodes (**d**).

467  $\Omega$  µm for planar, SOI and multigate low standby power CMOS, respectively), which is dominated by the contact resistance). We also found that the contact resistance decreases by another factor of three at a gate bias of +30 V, as shown in the inset of Fig. 2d. The improvement in device performance and reduction in contact resistance with 1T contacts is also highlighted in Fig. 2e,f. Clear nonlinear  $I_{\rm d}$ – $V_{\rm ds}$  characteristics indicative of Schottky behaviour of metal pads directly on 2H contacts can be seen in Fig. 2e whereas ohmic-like behaviour (linear  $I_{\rm d}$ – $V_{\rm ds}$ ) is observed in Fig. 2f.

To translate the low contact resistances into device performance, we fabricated FETs with 1T phase source and drain electrodes and the 2H phase as the channel material. Both top- and bottomgated devices were investigated and their properties measured in air. The 1T electrode devices always performed better in both configurations. The transfer characteristics of the bottom- and topgated devices with and without 1T phase electrodes are shown in Fig. 3a,b. Large gate modulation of the channel can be seen, with on/off ratios of >106 in bottom-gated devices. It is immediately noticeable that the saturation currents with 1T phase electrodes are approximately three times higher than in devices with Au electrodes, which translates into slightly higher on/off ratios. The drive currents achieved in devices with 1T electrodes is 85 µA µm<sup>-1</sup>, despite the MoS<sub>2</sub> channel being only 2-3 monolayers thick. In comparison,  $30\,\mu A\,\mu m^{-1}$  was achieved for devices with Au pads deposited directly on the 2H phase. As well as the very high drive currents, the transconductance value increased from  $\sim$ 110  $\mu A V^{-1}$  to 502  $\mu A V^{-1}$ in the 1T phase electrode devices. These FET properties measured in air and without any encapsulation layer manifest into enhanced field-effect mobility values of  $\sim 50 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  for the 1T phase electrode devices compared to  $\sim 15-20\,\mathrm{cm^2\,V^{-1}\,s^{-1}}$  for the 2H

Property	2H phase contacts	1T phase contacts	Ratio
On currents ( $\mu$ A $\mu$ m <sup>-1</sup> )	30	85	2.8
Transconductance ( $\mu$ S $\mu$ m <sup>-1</sup> )	1.4	3.8	2.7
Mobility (cm $^2$ V $^{-1}$ s $^{-1}$ )	19	46	2.5
On/off ratio	10 <sup>7</sup>	10 <sup>8</sup>	10
Subthreshold swing (V/decade)	1.5	0.8	0.5

contacts. The mobility values reported here can be further improved by elimination of any organic residues that might be present on the surface of  $MoS_2$  as well as optimization of dielectric deposition and annealing procedures. The bottom-gate device characteristics are summarized in Table 1.

Top-gated devices were also fabricated and tested with 1T electrodes. We investigated a variety of gate dielectrics (HfO $_2$ , SiO $_2$ , Al $_2$ O $_3$  and Si $_3$ N $_4$ ) on top of ultrathin MoS $_2$  nanosheets. We first attempted to deposit HfO $_2$  using ALD and obtained reasonably good quality devices (see Supplementary Information for details). However, we found that the use of Si $_3$ N $_4$  produced by PECVD as the gate dielectric also yielded highly reproducible, high-performance devices. Transfer characteristics of top-gated devices with and without 1T phase electrodes are shown in Fig. 3b. As with the back-gated devices, 1T electrodes enhance the performance of top-gated devices. In particular, excellent current saturation can be seen and the subthreshold swing values for the top-gated devices

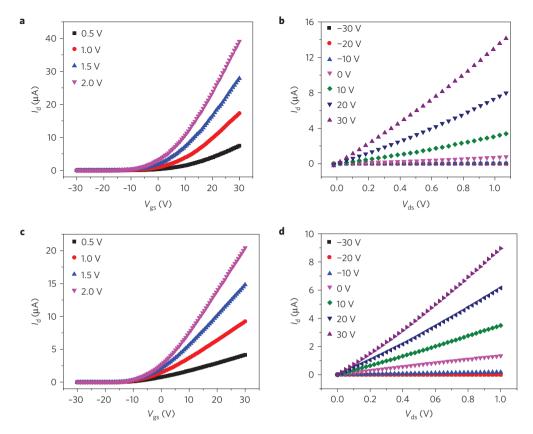


Figure 4 | Influence of the metal electrode work function on FET properties. a,b, Transfer (with  $V_{ds}$  ranging from 0.5 V to 2.0 V) and output (with  $V_{gs}$  ranging from -30 V to 30 V) characteristics, respectively, for devices with Pd deposited on top of 1T electrodes. **c,d**, Transfer and output characteristics, respectively, for devices with Ca deposited on top of 1T electrodes. The device properties are not substantially influenced by the work function of the metals used.

with 1T electrodes were found to be consistently in the range 90-100 mV/decade. In contrast, devices with Au directly on the 2H phase MoS<sub>2</sub> were found to be approximately 150 mV/decade. The differences in subthreshold swing between the two types of devices may be surprising since it depends on the channel capacitance, the capacitance of the dielectric, and capacitance from interface charges. All of these are expected to be similar in both devices. One reason for the lower subthreshold swing values in 1T devices could be the lower interface trap density, since the interface between the 1T and 2H phase is atomically sharp and the carrier density in the 1T phase is large. Another reason is that the actual channel length in the 1T phase devices is lower than the assumed value. This is because we have found that the butyl lithium diffuses into the channel under the PMMA so that some portion of the channel in the masked region is also converted to the 1T phase. As well as the shorter channel length, another advantage of the 1T electrodes could be that the source and drain electrodes are side contacts rather than vertical contacts. It has been discussed that side contacts could lead to better device properties in TMDs (refs 5,25). The saturation currents were also substantially larger in the 1T electrode devices  $(16 \,\mu\text{A}\,\mu\text{m}^{-1})$  compared to  $3 \,\mu\text{A}\,\mu\text{m}^{-1}$  on the non-phase-engineered electrodes. The lower drive currents in top-gated devices compared to back-gated devices is expected owing to underlap between gate electrode and source/drain. The absence of overlap means minimal barrier modulation and thus lower charge injection. The on/off ratio of both devices was found to be  $>10^7$ . Mobility values for top-gated devices have been shown to be substantially lower than back-gated devices<sup>54</sup>. We obtain values of  $\sim$ 12–15 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> for 1T metallic electrodes compared to 3-5 cm<sup>2</sup> V<sup>-1</sup> s<sup>-1</sup> for Au on 2H electrodes. The top-gate device characteristics are summarized in Table 2.

Table 2   Comparison of top-gated devices.
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Property	2H phase contacts	1T phase contacts	Ratio
On currents (μA μm <sup>-1</sup> )	3	16	5.3
Transconductance (μS μm <sup>-1</sup> )	1.1	3.1	2.8
Mobility (cm $^2$ V $^{-1}$ s $^{-1}$ )	3.5	12.5	3.7
On/off ratio	10 <sup>6</sup>	10 <sup>7</sup>	10
Subthreshold swing (mV/decade)	150	95	0.6

To demonstrate that the true contact in the FET devices is between the 1T phase electrodes and the 2H phase channel, we investigated metal pads of varying work functions. As well as the Au metal pads used in the measurements reported thus far, we also tested calcium and palladium—low- and high-workfunction metals. We found that reproducible FETs were challenging to fabricate when source/drain electrodes from these metals were directly deposited on to the 2H phase. For the working devices, the properties with Pd and Ca electrodes were relatively poor (see Supplementary Information for details) when deposited directly onto the 2H phase. In contrast, we found that highly reproducible devices with consistent properties in terms of mobility  $(20-30 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1})$ , saturation currents  $(30 \,\mu\text{A}\,\mu\text{m}^{-1})$  and on/off (>10<sup>7</sup>) ratio can be produced when metal pads are deposited on phase-engineered 1T electrodes. The FET transfer and output characteristics of back-gated devices with Ca and Pd metal pads deposited on the 1T phase are shown in Fig. 4. The fact that both devices perform reasonably similarly at room temperature despite the large differences in the metal work functions suggests that the ARTICLES NATURE MATERIALS DOI: 10.1038/NMAT4080

barrier for charge injection into the channel is at the 1T/2H interface and not at the metal/1T interface.

It is also worth noting that devices fabricated with 1T phase electrodes are highly reproducible and independent of the type of electrode metal used. In this study, we have fabricated and tested hundreds of devices with 1T electrodes; the yield of these devices is nearly 100% with consistent performance. In contrast, the yield of working devices fabricated with metals on top of the 2H phase was substantially lower and device characteristics were highly variable. The 1T phase is metastable, but we have demonstrated that it is stable under environmental conditions and also as catalyst for hydrogen evolution—however, its stability under high-performance device operation remains to be elucidated.

In summary, we have shown that phase engineering can markedly reduce the contact resistance between the source/drain electrodes and the channel to enable high-performance FETs. Specifically, we demonstrate that the metallic 1T phase is an effective contact electrode with record low-resistance values of  $200\,\Omega\,\mu m$  at zero gate bias. The low contact resistance leads to unprecedentedly high drive currents (85  $\mu A\,\mu m^{-1}$ ), high mobility values, 95 mV/decade subthreshold swing values, and on/off ratios greater than  $10^7$ . The excellent device properties we obtain are for a 1T phase concentration of  $\sim\!\!70\%$ , suggesting that conversion to the pure 1T phase could lead to even greater enhancement in performance. Our work shows that phase engineering of electrodes is an effective strategy for further improving the performance of  $MoS_2$  devices.

#### Methods

**Local 1T phase transformation.** After identifying the flakes on which the devices were to made, PMMA (C4 from Microchem) was spin-coated onto the sample at 3,000 r.p.m. for 60 s, followed by baking at 180 °C for 90 s. This was followed by e-beam lithography to remove PMMA from the portion(s) of the flake where 1T conversion was desired. To perform the phase transformation of the material, samples were immersed into 5 ml of 1.6 M *n*-butyl lithium (Sigma Aldrich) for two hours. All the butyl lithium exposure was done in a glove box in argon atmosphere at room temperature. Raman spectroscopy and XPS were used to confirm the phase transformation of MoS<sub>2</sub>. The lithium was removed by thoroughly washing the samples.

**Mobility extraction.** The slope of the FET transfer characteristic in the linear region gives us the transconductance  $(g_m)$  of the device, which is the change in the drain–source current when the gate voltage is varied. This was substituted into the mobility formula obtained by taking a first-order derivative of the drain–source current equation in the linear mode of FET operation.

$$\mu = \frac{Lg_{\rm m}}{WC_{\rm G}V_{\rm ds}}$$

where  $C_G$  is the back-gate capacitance. By inserting the appropriate values of the length (L) and width (W) of the device and the corresponding transconductance  $(g_m)$  at a particular  $V_{ds}$ , the mobility is obtained.

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NATURE MATERIALS DOI: 10.1038/NMAT4080 ARTICLES

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## **Author contributions**

M.C. conceived the idea, designed the experiments, analysed the data and wrote the manuscript. R.K., D.V. and A.D.M. conceived the idea and designed the experiments with M.C., synthesized the materials, fabricated the devices, made the measurements and analysed the data. S.E.Y. performed the AFM, EFM and PL mapping measurements. B.B. performed the gate dielectric depositions. G.G. helped to analyse the data and assisted in optimizing the 1T phase transformation chemistry. All the authors have read the manuscript and agree with its content.

### **Additional information**

Supplementary information is available in the online version of the paper. Reprints and permissions information is available online at www.nature.com/reprints. Correspondence and requests for materials should be addressed to A.D.M. or M.C.

## **Competing financial interests**

The authors declare no competing financial interests.